

Answers to Concrete Field and Concrete Plant Study Questions and Problems

CHAPTER 1 – for Concrete Field and Concrete Plant

- 1. **Hydration** is the chemical reaction between water and cement.
- 2. **Workability** is the property of freshly mixed concrete which is the ease or difficulty in the placing and finishing of concrete.
- 3. A chemical, such as calcium chloride used to "speed up" the setting time of concrete is accelerator.
- 4. **False set** is a significant loss of plasticity shortly after the concrete is mixed.
- 5. The time it takes a cement paste to begin hardening is known as **setting time**.
- 6. A condition at which an aggregate will neither absorb moisture from concrete nor contribute moisture to the mix is **saturated surface dry**.
- 7. <u>Set retarder</u> is a material used for the purpose of delaying the setting time of concrete.
- 8. **Consistency** is a condition of plastic concrete which relates to its cohesion, wetness, or to flow.
- 9. **Cement** is the bonding agent used in a concrete mix.
- 10. The ability of hardened concrete to resist the deterioration caused by weathering, chemicals, and abrasion is known as **durability**.
- 11. The pH value of water used with cement shall be between <u>4.5</u> and <u>8.5</u> as found in Section **216.02**.
- 12. Gypsum is added to cement to control **time of set**.
- 13. List two desirable qualities of hardened concrete: <u>durability and water-tightness</u> (others listed on page 1-1).
- 14. The primary effect of air entrainment in concrete is to improve <u>freeze thaw</u> <u>resistance</u>.
- 15. List two desirable properties of an aggregate: <u>low absorption and abrasive</u> resistance (others listed on pages 1-6 to 1-8).

16. Admixtures shall be dispensed <u>according to manufacturer recommendations and</u> within an accuracy of +/-3%.

- 17. List two principal raw components in the manufacture of cement: <u>Lime and Silica</u>.
- 18. The type of cement which has the highest fineness reading and the highest tricalcium silicate (C3S) composition, both factors in accelerated strength is **Type III.**
- 19. The void content of identically graded fine aggregates will vary with particle shape.
- 20. <u>3.15</u> is the specific gravity of Portland Cement.
- 21. <u>Water-cement ratio</u> has the greatest effect on the strength, durability and water tightness of concrete.
- 22. If the amount of admixture is constant and the concrete temperature is increased, the entrained air content will **decrease**.
- 23. A pH value of 6.0 indicates <u>acidity</u> and a pH value of 7.5 indicates <u>alkalinity</u>.
- 24. The strength requirements for High Early Strength Portland Cement Concrete shall be obtained in **7 days** as stated in Section **217.08(b)**.
- 25. In no case shall a vibrator be operated longer than <u>15</u> seconds in any one location as stated in Section <u>316.04(e)</u>.
- 26. The specification requirements for the approval to use admixtures in Hydraulic Cement Concrete are found in Section **215.03**.
- 27. Each batch of concrete shall be delivered to the site of work and discharged within **90 minutes** of the time the cement is introduced into the mixture unless approved otherwise by the Engineer as found in Section **217.09(b)**.
- 28. According to Section <u>217.10</u>, in cold weather, <u>water and aggregates</u> may be heated; however, <u>cement</u> is not to be heated.
- 29. Is Wash water from hydraulic cement concrete mixer operations is permitted to be reused in the concrete mix? **Yes, according to Section 216.02.**

CHAPTER 2 – Concrete PLANT

Sieve Analysis - No. 1

Check the following sieve analysis of a sample of natural sand for use in concrete subject to abrasion and determine if it meets Virginia Department of Transportation requirements for Grading "A" Sand. Circle the sieve not passing, if any.

Sieve	Cumulative	Cumulative		VDOT Specs.
Size	Grams Retained	%Retained	%Passing	(%Passing)
3/8 inch	0.0	0.0	100.0	100
No. 4	16.6	2.9	97.1	95-100
No. 8	64.5	11.3	88.7	80-100
No. 16	214.1	37.4	62.6	50-85
No. 30	389.2	67.9	32.1	25-60
No. 50	483.0	84.3	15.7	5-30
No. 100	543.4	94.8	5.2	0-10
No. 200	565.0	98.6	1.4	0-3
Total Wt.	<u>573.0</u>			

What is the Fineness Modulus? 2.99

$$\frac{0.0+2.9+11.3+37.4+67.9+84.3+94.8}{100} = \frac{2.99}{100}$$

Sieve Analysis - No. 2

Check the following sieve analysis of a sample of natural sand for use in concrete subject to abrasion and determine if it meets Virginia Department of Transportation requirements for Grading "A" Sand. Circle the sieve not passing, if any.

Sieve Size	Cumulative Grams Retained	Cumulative %Retained	%Passing	VDOT Specs. (%Passing)
3/8 inch	0.0	0.0	100.0	<u>100</u>
No. 4	6.9	1.4	98.6	95-100
No. 8	28.3	5.6	94.4	80-100
No. 16	34.9	6.9	93.1	50-85
No. 30	219.2	43.6	56.4	25-60
No. 50	398.8	79.3	20.7	5-30
No. 100	482.9	96.0	4.0	0-10
No. 200	498.1	99.0	1.0	0-3
Total Wt.	<u>503.0</u>			

Yes	No	XX

$$\frac{0.0+1.4+5.6+6.9+43.6+79.3+96.0}{100} = \frac{232.8}{100} = \frac{\textbf{2.33}}{100}$$

Sieve Analysis - No. 3

Check the following sieve analysis of a sample of natural sand for use in concrete not subject to abrasion and determine if it meets Virginia Department of Transportation requirements for Grading "A" Sand. Circle the sieve not passing, if any.

Sieve Size	Cumulative Grams Retained	Cumulative %Retained	%Passing	VDOT Specs. (%Passing)
3/8 inch	0.0	0.0	100.0	100
No. 4	6.7	1.4	98.6	95-100
No. 8	54.0	11.3	88.7	80-100
No. 16	168.6	35.1	64.9	50-85
No. 30	340.5	70.9	29.1	25-60
No. 50	407.7	84.9	15.1	5-30
No. 100	459.1	95.6	4.4	0-10
No. 200	468.1	97.5	2.5	0-5
Total Wt.	<u>480.0</u>			

Yes	XX	No	

What is the Fineness Modulus? 2.99

$$\frac{0.0+1.4+11.3+35.1+70.9+84.9+95.6}{100} = \frac{299.2}{100} = \frac{2.99}{100}$$

CHAPTER 3 – Concrete PLANT

ACI MIX DESIGN PROBLEM NO. 1

			CLASS A4	MI	IX DESIG	N MODII	FIED		
			WITH_ Fly	ash		20122			
	AGGREGATE						AGGREGA		
F.M.	2.70		_		Ι	DRY ROD	DED UNI	T WT. 10	03 lb/ft ³ _
SP. G	R. 2.64				S	SP. GR.		2.63	
NOMINA	AL MAX. SI	ZE C.A.	1 inch	_	7	TABLE A	1.5.3.6	FACTOR _	0.68
OTHER	DATA NEED	ED FOR S	SPECIAL DE	SIGNS	Flyash	20% Re	placeme	nt	
QUANT: TABLE	ITY OF COA A1.5.3.6	RSE AGGI 0.68	REGATE X 27		Sp. Gr.			1891	lbs.
			ABS	OLUT	E VOL	UMES			
PORTL	AND CEMENT	.20 x 6	535 = 127	635 - 3.	127 = 5 15 x 62	508 lbs	. = _	2.58	ft [:]
WATER				.45 x	635 = 2 1.00 x	2 86 lbs	<u>. </u>	4.58	ft²
AIR				6	100	- % X	27 = _	1.76	ft ²
C. AG	GR.			1 SP.G	891 R. 2.63	lbs X 6	· = _	11.52	ft [:]
ADDIT	IONAL MATE	RIALS		.20	x 635 =	= 127 52.4	=	0.87	ft [:]
	27.00	ft^3			כ	ΓΟΤΑL	=	21.31	ft ³
-	21.31	ft^3							
F.A	5.69	ft³ X	2.64	SP.	.GR. X	62.4	=	937	lbs.
SUGGE	STED QUANT	ITIES			Ⅎ	± 5% TO	LERANCE		
	CEMENT		508		kg				
	WATER	286	lbs. or	34	. 3 ga	als.			
	AIR		6.5		%				
	C. AGGR.		1891		lbs.	- [_] + []
	F. AGGR.		937		lbs.] + [
	ADDL. MAT	LS. Flya	ash = =	127 lb	s.				

ACI MIX DESIGN PROBLEM NO. 2

CLASS A4 General MIX DESIGN MODIFIED WITH COARSE AGGREGATE FINE AGGREGATE F.M. 3.0 DRY RODDED UNIT WT. 1051b/ft3_ SP. GR. 2.64 SP. GR. 2.83 NOMINAL MAX. SIZE C.A. 1 inch TABLE A1.5.3.6 FACTOR 0.65 OTHER DATA NEEDED FOR SPECIAL DESIGNS Sp.Gr. of IP 3.02 QUANTITY OF COARSE AGGREGATE TABLE A1.5.3.6 _____ X 27 ft³ X UNIT WT. ____ 105 ___ = ____ 1843 ____ lbs. ABSOLUTE VOLUMES ΤP $\frac{635}{3.15 \times 62.4} \quad \text{lbs.} = \frac{3.37}{5.37} \text{ ft}^{3}$ PORTLAND CEMENT $.45 \times 635 = 286$ lbs. = 4.58 ft³ WATER 1.00 x 62.4 $\frac{\textbf{6.5}}{100} \% \times 27 = \frac{\textbf{1.76}}{} \text{ft}^{3}$ AIR 1843 | lbs. = 10.44 | ft³ SP.GR. 2.83 | X 62.4 C. AGGR. = ft³ ADDITIONAL MATERIALS ft³ = **20.15** ft³ TOTAL 27.00 ft³ - **20.15** ft³ F.A. 6.85 ft³ X 2.64 SP.GR. X 62.4 = 1128 lbs. ± 5% TOLERANCE SUGGESTED QUANTITIES CEMENT _____ 635 lbs. WATER _____ 1bs. or ____ 34.3 __gals. AIR 6.5 _____ lbs. - [_____] + [] C. AGGR. 1843 F. AGGR. 1128 lbs. - [] + [] ADDL. MATLS. =

ACI MIX DESIGN PROBLEM NO. 3

CLASS A4 Post & Rail MIX DESIGN MODIFIED WITH Slag COARSE AGGREGATE FINE AGGREGATE F.M. 2.7 DRY RODDED UNIT WT. 101 lb/ft3_ SP. GR. 2.62 SP. GR. 2.62 NOMINAL MAX. SIZE C.A. 1/2 inch TABLE A1.5.3.6 FACTOR 0.56 OTHER DATA NEEDED FOR SPECIAL DESIGNS Slag 40% Replacement (Sp. Gr. 2.94) w/c 0.43 QUANTITY OF COARSE AGGREGATE ABSOLUTE VOLUMES PORTLAND CEMENT .40 x 635 = 254 635 - 254 = 381 lbs. = 1.94 ft³ $3.1\overline{5} \times 62.4$ $.43 \times 635 = 273$ lbs. = 4.38 ft³ WATER AIR 7.0 % x 27 = 1.89 ft³ lbs. = 9.34 ft³ C. AGGR. 1527 lbs SP.GR. 2.62 X 62.4 $635 \times .40 = 254 = 1.38$ ft³ ADDITIONAL MATERIALS 40% Slag 2.94 x 62.4 = ____ ft³ = ____**18.93** ft³ TOTAL 27.00 ft³ - 18.93 ft³ F.A. 8.07 ft³ X 2.62 SP.GR. X 62.4 = 1319 lbs. ± 5% TOLERANCE SUGGESTED QUANTITIES CEMENT _____ lbs. WATER _ 273 lbs. or 32.8 gals. 7.0 % AIR C. AGGR. **1527** lbs. - [] + [] _____ lbs. - [] + [] F. AGGR. 1319 ADDL. MATLS. Slag = 254 lbs.

ACI MIX DESIGN PROBLEM NO. 4 - MODIFIED WITH FLY ASH

	CLASS _A	4 General	MIX	DESIGN		
FINE AGGREGATE	MOI	OIFIED WITH	Fly As COARSE	h AGGREGAT	ſE	
F.M. 3.0			DRY ROD	DED UNIT	г WT. 105 lb	/ft <u>³</u> _
SP. GR. 2.64			SP. GR.		3.04	
NOMINAL MAX. SIZE C	.A. <u>1 incl</u>	1	TABLE A	1.5.3.6	FACTOR 0.6	5
OTHER DATA NEEDED FO	OR SPECIAL I					
QUANTITY OF COARSE ATABLE A1.5.3.60	AGGREGATE .65 X 2		Sp. Gr			lbs.
	AB	SOLUTE	VOLUME	ES		
PORTLAND CEMENT .20	x 635 = 12	7 635 <u>- 127</u> 3.15 x	$\frac{7 = 508}{62.4}$	bs. =	2.58	ft³
WATER	.45	x 635 = 2 1.00 x 6	86 lbs.	= _	4.58	ft³
AIR		6.5	% x 27 100	=	1.76	ft³
C. AGGR.	Ç	1843 SP.GR. 3.04	lbs. L X 62	- 4	9.72	ft³
ADDITIONAL MATERIAL:	5	635 x .20 2.35 x 6	= 127	=	0.87 ft ³	ft³
27.00 ft ³					19.51	ft³
- <u>19.51</u> ft ³						
F.A7.49 ft ³	X2.64	SP.GR.	X 62.4	4 =	1234	lbs.
SUGGESTED QUANTITIES			±	5% TOLE	ERANCE	
CEMENT	508		lbs.			
WATER286	lbs. c	or <u>34.3</u>	gals.			
AIR	6.5		ଚ			
C. AGGR.	1843		lbs	[]] + []
F. AGGR.	1234		lbs	[]] + []
ADDL. MATLSI	Fly Ash = =	127 lbs.	-			

ACI MIX DESIGN PROBLEM NO. 5

CLASS <u>A4 General</u> MIX DESIGN MODIFIED WITH FINE AGGREGATE COARSE AGGREGATE F.M. 2.8 DRY RODDED UNIT WT. 100 lb/ft3-_ SP. GR. 3.04 SP. GR. <u>2.</u>64 NOMINAL MAX. SIZE C.A. 1 inch TABLE A1.5.3.6 FACTOR 0.67 OTHER DATA NEEDED FOR SPECIAL DESIGNS IS Sp. Gr. 3.05 QUANTITY OF COARSE AGGREGATE TABLE A1.5.3.6 0.67 X 27 ft³ X UNIT WT. 100 = 1809 lbs. ABSOLUTE VOLUMES 635 lbs. = 3.34 ft³ PORTLAND CEMENT 3.05 x 62.4 $.45 \times 635 = 286$ lbs. = 4.58 ft³ WATER 1.00 x 62.4 6.5 % x 27 = 1.76 ft³ AIR $\frac{1809}{\text{SP.GR.} \ 3.04} \quad \text{1bs.} = \frac{9.54}{62.4} \text{ft}^{3}$ C. AGGR. ADDITIONAL MATERIALS TOTAL = 19.22 ft³ 27.00 ft³ - 19.22 ft³ F.A. 7.78 ft³ X 2.64 SP.GR. X 62.4 = 1282 lbs. SUGGESTED QUANTITIES ± 5% TOLERANCE CEMENT 635 lbs. WATER 286 lbs. or 34.3 gals. 6.5_____ % AIR C. AGGR. 1809 lbs. - [] + [1282 lbs. - [____] + [___ F. AGGR. ADDL. MATLS. =

ACI MIX DESIGN PROBLEM NO. 6

CLASS A3 General MIX DESIGN MODIFIED WITH Slag COARSE AGGREGATE FINE AGGREGATE F.M. 3.0 DRY RODDED UNIT WT. 99 lb/ft^{3} SP. GR. 2.64 SP. GR. 2.62 NOMINAL MAX. SIZE C.A. 1 inch TABLE A1.5.3.6 FACTOR 0.65 OTHER DATA NEEDED FOR SPECIAL DESIGNS 40% Slag Replacement (Sp. Gr. 2.94) QUANTITY OF COARSE AGGREGATE TABLE A1.5.3.6 0.65 X 27 ft³ X UNIT WT. 99 = 1737 lbs. ABSOLUTE VOLUMES PORTLAND CEMENT .40 x 588 = 235 588 - 235 = 353 lbs. = 1.80 ft³ 3.15 x 62.4 $\frac{.49 \times 588 = 288}{1.00 \times 62.4} \text{ lbs.} = \frac{4.62}{1.00 \times 62.4} \text{ ft}^{3}$ WATER AIR $\frac{1737}{\text{SP.GR.} \ 2.62} \frac{1\text{bs.}}{\text{X 62.4}} = \frac{10.62}{\text{ft}^3}$ C. AGGR. $.40 \times 588 = 235 \text{ lbs.} = 1.28 \text{ ft}^3$ ADDITIONAL MATERIALS 2.94 x 62.4 TOTAL = 19.94 ft³27.00 ft³ - 19.94 ft³ F.A. 7.06 ft³ X 2.64 SP.GR. X 62.4 = 1163 lbs. ± 5% TOLERANCE SUGGESTED QUANTITIES CEMENT _____ 353 lbs. WATER 288 lbs. or <u>34.6</u> gals. 6.0 % C. AGGR. 1737 lbs. - [____] + [____] F. AGGR. 1163 lbs. - [] + [] ADDL. MATLS. Slag = 235 lbs.

ACI MIX DESIGN PROBLEM NO. 7

CLASS A3 Paving MIX DESIGN MODIFIED WITH Slag FINE AGGREGATE COARSE AGGREGATE F.M. _ 2.7 DRY RODDED UNIT WT. 104 lb/ft³_ SP. GR. 2.64 SP. GR. 2.60 NOMINAL MAX. SIZE C.A. 1 inch TABLE A1.5.3.6 FACTOR 0.68 OTHER DATA NEEDED FOR SPECIAL DESIGNS 50% Slag Replacement (Sp. Gr. 2.94) QUANTITY OF COARSE AGGREGATE TABLE A1.5.3.6 0.68 X 27 ft 3 X UNIT WT. 104 = 1909 lbs. ABSOLUTE VOLUMES PORTLAND CEMENT .50 x $564 = 282 \ 564 - 282 = 282 \ lbs. = 1.43$ ft³ 3.15 x 62.4 $\frac{.49 \times 564 = 276}{1.00 \times 62.4}$ lbs. = $\frac{4.42}{1.00 \times 62.4}$ WATER 6.0 % x 27 = 1.62 ft³ ATR 1909 1909 lbs. SP.GR. 2.60 X 62.4 C. AGGR. = 11.77 ft³ $\frac{564 \times .50 = 282}{2.94 \times 62.4} = \frac{1.54}{}$ ft³ ADDITIONAL MATERIALS 50% Slag ft³ = 20.78 ft³ TOTAL 27.00 ft³ -20.78 ft³ F.A. 6.22 ft³ X 2.64 SP.GR. X 62.4 = 1025 lbs. ± 5% TOLERANCE SUGGESTED QUANTITIES CEMENT ____ 1bs. WATER 276 lbs. or 33.1 gals. 6.0 _____ % _____ lbs. - [_____] + [C. AGGR. ____ 1909 F. AGGR. 1025 lbs. - [____] + [____ ADDL. MATLS. Slag = 282 lbs.

ACI MIX DESIGN PROBLEM NO. 8 - MODIFIED WITH FLY ASH

CLASS A3 General MIX DESIGN MODIFIED WITH Fly Ash FINE AGGREGATE COARSE AGGREGATE F.M. ____ 2.8 DRY RODDED UNIT WT. 105 lb/ft3_ SP. GR. 2.63 SP. GR. 2.64 NOMINAL MAX. SIZE C.A. 1 inch TABLE A1.5.3.6 FACTOR 0.67 OTHER DATA NEEDED FOR SPECIAL DESIGNS 20% Fly Ash Replacement Sp. Gr. 2.22 QUANTITY OF COARSE AGGREGATE TABLE A1.5.3.6 _____ X 27 ft³ X UNIT WT. ____ 105 ___ = ____ 1899 ___ lbs. ABSOLUTE VOLUMES $588 \times .80 = 470$ lbs. = 2.39 ft³ PORTLAND CEMENT 3.15 x 62.4 WATER $.49 \times 588 = 288$ lbs. = 4.62 ft³ 1.00 x 62.4 6.0 % x 27 = 1.62 ft³ ATR C. AGGR. 1899 lbs. = 11.57 ft³ SP.GR. 2.63 X 62.4 $\frac{588 \times .20 = 118}{2.22 \times 62.4}$ = 0.85 ft³ ADDITIONAL MATERIALS ft³ = 21.05 ft³ TOTAL 27.00 ft³ - 21.05 ft³ F.A. 5.95 ft³ X 2.64 SP.GR. X 62.4 = 980 lbs. SUGGESTED QUANTITIES ± 5% TOLERANCE CEMENT 470 lbs. WATER 288 kg or 34.6 gals. ____6.0 % AIR C. AGGR. ____ 1899 lbs. - [] + [] F. AGGR. 980 lbs. - [____] + [____] ADDL. MATLS. Fly Ash = 118 lbs.

ACI MIX DESIGN PROBLEM NO. 9 - MODIFIED WITH FLY ASH

CLASS A4 General MIX DESIGN MODIFIED WITH Fly Ash COARSE AGGREGATE FINE AGGREGATE F.M. ____ 3.0 DRY RODDED UNIT WT. 98 lb/ft³_ SP. GR. 2.62 SP. GR. 2.64 NOMINAL MAX. SIZE C.A. 1 inch TABLE A1.5.3.6 FACTOR 0.65 OTHER DATA NEEDED FOR SPECIAL DESIGNS 25% Fly Ash Replacement Sp. Gr. 2.30 QUANTITY OF COARSE AGGREGATE TABLE A1.5.3.6 0.65 X 27 ft³ X UNIT WT. 98 = 1720 lbs. ABSOLUTE VOLUMES PORTLAND CEMENT $.25 \times 635 = 159$ 635 - 159 = 476 lbs. = 2.42 ft³ 3.15 x 62.4 WATER $.45 \times 635 = 286 \text{ lbs.} = 4.58 \text{ ft}^3$ 1.00 x 62.4 $\frac{6.5}{100}$ % x 27 = $\frac{1.76}{100}$ ft³ ATR $\frac{1720}{\text{SP.GR.}} \times \frac{1720}{2.62} \times 62.4$ lbs. = $\frac{10.52}{}$ ft³ C. AGGR. $\frac{635 \times .25 = 159}{2.30 \times 62.4} = \frac{1.11}{2.30 \times 62.4}$ ADDITIONAL MATERIALS = _____ ft³ = 20.39 ft³ TOTAL 27.00 ft³ - 20.39 ___ ft³ F.A. 6.61 $ft^3 \times 2.64$ SP.GR. $\times 62.4 = 1089$ lbs. SUGGESTED QUANTITIES ± 5% TOLERANCE CEMENT ____ 1bs. WATER 286 lbs. or 34.3 gals. 6.5 % C. AGGR. 1720 lbs. - [] + [lbs. - [____] + [____ F. AGGR. 1089 ADDL. MATLS. Fly Ash = 159 lbs. ____ = ____

ACI MIX DESIGN PROBLEM NO. 10 - MODIFIED WITH SLAG

CLASS A4 Post & Rail MIX DESIGN

FINE AGGREGATE	MODIFIED	WITH Slag COARSE AGGRE	GATE	
F.M. 2.80		DRY RODDED U	JNIT WT. 102 lb,	<u>/ft³_</u>
SP. GR. 2.83		SP. GR	2.81	
NOMINAL MAX. SIZE C	C.A. <u>½ inch</u>	TABLE A1.5.3	3.6 FACTOR0.55	<u> </u>
OTHER DATA NEEDED F	OR SPECIAL DESIGNS	Slag 50% Replac	cement (Sp. Gr. 2	2.85)
QUANTITY OF COARSE TABLE A1.5.3.60		UNIT WT 102	_= _ 1515	lbs.
	ABSOLUT	E VOLUMES		
PORTLAND CEMENT 635	$5 \times .50 = 318 \frac{635 - }{3}$	$\frac{318 = 317}{.15 \times 62.4}$ lbs.	= 1.61	ft³
WATER	.45 x 635:	= 286 lbs.	= 4.58	ft³
AIR	7.0 100	% x 27 =	1.89	ft³
C. AGGR.	15: SP.GR.	15 lbs. 2.81 X 62.4	= 8.64	ft³
ADDITIONAL MATERIAL	uS 50% Slag <u>6</u> 3	$\frac{35 \times .50 = 318}{2.85 \times 62.4}$	= <u>1.79</u>	ft³ ft³
27.00 ft ³	_		= 18.51	
18.51 ft ³				
F.A8.49 ft ³	X <u>2.83</u> P.GR	a. x 62.4 =	1499	_ lbs.
SUGGESTED QUANTITIE	lS	± 5% T	COLERANCE	
CEMENT	317	lbs.		
WATER28	36 lbs. or <u>34</u>	.3 gals.		
AIR	7.0	%		
C. AGGR.	1515	lbs [] + []
F. AGGR		lbs [
ADDL. MATLS	Slag 50% = 318 :	lbs.		

ACI MIX DESIGN ADJUSTMENT PROBLEM NO. 1

The following Class A4 General Use mix design produced a harsh mix. The contractor wants to reduce the harshness. What are the maximum allowable adjustments under VDOT specifications that could be made to reduce the harshness?

Mix Design - One Cu. Yard Based on SSD Condition

IP Cement	635 lbs.	Sand - F. M.	2.80
Sand	1150 lbs.	Sand - Sp. Gr.	2.64
No. 57	1954 lbs.	CA - Sp. Gr.	3.04
Water	286 lbs.	CA – Unit Weight	108 lb/ft ³
Air	6.5 %	IP Cement - Sp. Gr. `	3.05

ANSWERS

Cement 635 lbs.

Sand <u>1208</u> lbs.

No. 57 <u>1888</u> lbs.

Water <u>286</u> lbs.

Air <u>6.5%</u> lbs.

$$1150 + 58 = 1208$$

$$0.35 \times 3.04 \times 62.4 = 66.0$$

ACI MIX DESIGN ADJUSTMENT PROBLEM NO. 2

The following Class A3 General Use mix design produced a harsh mix. The contractor wants to reduce the harshness. What are the maximum allowable adjustments under VDOT specifications that could be made to reduce the harshness?

Mix Design - One Cu. Yard Based on SSD Condition

IS Cement	588 lbs.	Sand - F. M.	2.70
Sand	983 lbs.	Sand - Sp. Gr.	2.66
No. 57	1909 lbs.	CA - Sp. Gr.	2.61
Water	288 lbs.	CA - Unit Weight	104 lb/ft ³
Air	6.0 %	IS Cement - Sp. Gr.	3.02

ANSWERS

Cement <u>588</u> lbs.

Sand <u>1032</u> lbs.

No. 57 <u>1860</u> lbs.

Water <u>288</u> lbs.

Air <u>6.0</u> %

CALCULATIONS:

SAND: 983 x 0.05 = 49.15

983 + 49 = 1032

NO 57: $\frac{49}{2.66 \times 62.4} = \frac{49}{165.984} = 0.30$

 $0.30 \times 2.61 \times 62.4 = 49$

1909 - 49 = 1860

ACI MIX DESIGN ADJUSTMENT PROBLEM NO. 3

The following Class A4 General Use mix design modified with 40% slag produced a harsh mix. The contractor wants to reduce the harshness. What are the maximum allowable adjustments under VDOT specifications that could be made to reduce the harshness?

Mix Design - One Cu. Yard Based on SSD Condition

Cement	381 lbs.	Sand - F. M.	2.70
Sand	1285 lbs.	Sand - Sp. Gr.	2.62
No. 57	1799 lbs.	CA - Sp. Gr.	3.04
Water	286 lbs.	CA - Unit Weight	98 lb/ft³
Air	6.5 %		
Slag	254 lbs.	Slag - Sp. Gr.	2.95

ANSWERS

Cement <u>381</u> lbs.

Sand <u>1349</u> lbs.

No. 57 <u>1725</u> lbs.

Air <u>6.5</u>%

Water <u>286</u> lbs.

Slag <u>254</u> lbs.

CALCULATIONS:

SAND: $1285 \times 0.05 = 64.25$

1285 + 64 = 1349

NO 57: <u>64</u> <u>64</u> 2.62 x 62.4 = 163.488 = 0.39

 $0.39 \times 3.04 \times 62.4 = 74$

1799 - 74 = 1725

ACI MIX DESIGN ADJUSTMENT PROBLEM NO. 4

The following Class A3 General Use Mix Design produced a 2 inch slump. The contractor wants a 3 inch slump. What are the maximum allowable adjustments under VDOT specifications that could be made to increase the slump as much as possible?

Mix Design - One Cu. Yard Based on SSD Condition

IP Cement	588 lbs.	Sand - F. M.	2.80
Sand	1107 lbs.	Sand - Sp. Gr.	2.64
No. 57	1934 lbs.	CA - Sp. Gr.	2.83
Water	288 lbs.	CA - Unit Weight	106.9 lb/ft ³
Air	6.0 %	IP Cement - Sp. Gr.	3.05

ANSWERS

Cement <u>588</u> lbs.

Sand <u>1052</u> lbs.

No. 57 <u>1992</u> lbs.

Water <u>288</u> lbs.

Air <u>6.0</u> %

$$0.33 \times 2.83 \times 62.4 = 58$$

ACI MIX DESIGN ADJUSTMENT PROBLEM NO. 5

The following Class A3 general use mix design modified with 20% flyash produced a 3 inch slump. The contractor wants a 4 inch slump. What are the maximum allowable adjustments under VDOT specifications that could be made to increase the slump as much as possible?

Mix Design - One Cu. Yard Based on SSD Condition

Cement	470 lbs.	Sand - F. M.	2.80
Sand	1120 lbs.	Sand - Sp. Gr.	2.83
No. 57	1863 lbs.	CA - Sp. Gr.	2.62
Water	288 lbs.	CA - Unit Weight	103 lb/ft ³
Air	6.0 %		
Flyash	118 lbs.	Flyash - Sp. Gr.	3.00

ANSWERS

Cement 470 lbs.

Sand <u>1064</u> lbs.

No. 57 <u>1915</u> lbs.

Water <u>288</u> lbs.

Air <u>6.0</u>%

Flyash <u>118</u> lbs.

CALCULATIONS:

SAND: $1120 \times 0.05 = 56$

1120 - 56 = 1064

NO 57: $\frac{56}{2.83 \times 62.4} = \frac{56}{176.592} = 0.32$

 $0.32 \times 2.62 \times 62.4 = 52$

1863 + 52 = 1915

ACI MIX DESIGN ADJUSTMENT PROBLEM NO. 6

The following Class A4 general use mix design produced a 2 inch slump. The contractor wants a 3 inch slump. What are the maximum allowable adjustments under VDOT specifications that could be made to increase the slump as much as possible?

Mix Design - One Cu. Yard Based on SSD Condition

IS Cement	635 lbs.	Sand - F. M. 2.90
Sand	1094 lbs.	Sand - Sp. Gr. 2.62
No. 57	1871 lbs.	CA - Sp. Gr. 2.83
Water	286 lbs.	CA - Unit Weight 105 lb/ft³
Air	6.5 %	IS Cement - Sp. Gr. 3.02

ANSWERS

SAND:
$$1094 \times 0.05 = 54.7$$

$$0.34 \times 2.83 \times 62.4 = 60$$

CHAPTER 9 – Concrete PLANT

MOISTURE PROBLEM NO. 1

A. Given the following information, determine the percent of free moisture in the sand and No. 57.

SAND

Weight of wet sample = 635 grams Weight of dry sample = 598 grams

NO. 57

Weight of wet sample = 1240 grams Weight of dry sample = 1220 grams

ABSORPTION

Sand = 0.6%No. 57 = 0.2%

Free Moisture: Sand <u>5.6%</u> No. 57 <u>1.4%</u>

Sand:
$$635$$
 $\frac{37}{598}$ $x 100 = 6.2$ $\frac{-0.6}{5.6\%}$

No. 57 1240 $\frac{20}{20}$ 1220 $x 100 = 1.6$ $\frac{-0.2}{1.4\%}$

B. Based on the preceding moisture determination, correct the following mix design weights to batch weights or "pull weights" for one cubic yard.

Mix Design - One Cubic Yard Based on SSD Condition

Batch Quantities

Sand	<u>1127</u> lbs.
No. 57 _	<u>1861</u> lbs.
Water	<u>202</u> lbs.
	No. 57 _

<u>24.2</u> gals. Air 6.5 % Air <u>6.5 %</u>

CALCULATIONS:

Water:
$$60 + 26 = 86$$

8.33

MOISTURE PROBLEM NO. 2

A. Given the following information, determine the percent of free moisture in the sand and No. 57.

SAND

Weight of wet sample = 628 grams Weight of dry sample = 582 grams

NO. 57

Weight of wet sample = 1245 grams Weight of dry sample = 1215 grams

ABSORPTION

Sand = 0.9%No. 57 = 0.4%

Free Moisture: Sand <u>7.0%</u> No. 57 <u>2.1%</u>

B. Based on the preceding moisture determination, correct the following mix design weights to batch weights or "pull weights" for one cubic yard.

Mix Design - One Cubic Yard Based on SSD Condition

Batch Quantities

Cement	635 lbs.	Cement	635	lbs.

Sand:
$$1070 \times 0.070 = 75$$

$$1840 + 39 = 1879$$

Water:
$$75 + 39 = 114$$

MOISTURE PROBLEM NO. 3

A. Given the following information, determine the percent of free moisture in the sand and No. 57.

SAND

Weight of wet sample = 621 grams Weight of dry sample = 580 grams

NO.57

Weight of wet sample = 1362 grams Weight of dry sample = 1343 grams

ABSORPTION

Sand = 0.7%No. 57 = 0.4%

Free Moisture: Sand <u>6.4%</u> No. 57 <u>1.0%</u>

Sand:
$$621$$
 41 7.1 -580 41 $580 \times 100 = 7.1$ -0.7 6.4

No. 57 1362
$$\underline{19}$$
 1.4 $\underline{-1343}$ 1343 x 100 = 1.4 $\underline{-0.4}$ 1.0

B. Based on the preceding moisture determination, correct the following mix design weights to batch weights or "pull weights" for four cubic yards.

Mix Design - One Cubic Yard Based on SSD Condition

Batch Quantities

Cement 635 lbs. Cement <u>2540</u> lbs.

Sand 1070 lbs. Sand <u>4552</u> lbs.

No. 57 1840 lbs. No. 57 <u>7432</u> lbs.

Water 286 lbs. Water <u>800</u> lbs.

<u>96.0</u> gals.

Air 7.0 % Air <u>7.0 %</u>

CALCULATIONS:

Sand: $1070 \times 0.064 = 68$

 $(1070 + 68) \times 4 = 4552$

No. 57: 1840 x 0.010 = 18 (1840

+ 18) x 4 = 7432

Water: 68 + 18 = 86

 $(286 - 86) \times 4 = 800$

800 = 96.0 gals.

8.33

Cement: 635 X 4 = 2540

CHAPTER 5 – Concrete PLANT

1. Before any concrete is batched, the producer's technician should determine that there is an approved <u>mixdesign</u> at the plant.

- 2. The required weighing accuracy for cement is **1 percent**.
- 3. Aggregates arriving at a plant by truck are acceptable for use if they are accompanied by a **statement ofcertification**.
- 4. Hopper and cement scales for batching concrete materials must be **servicedby a Private Scale Company**.
- 5. Aggregates should be handled and stockpiled in such a manner as to minimize <u>segregation</u>.
- 6. The required weighing accuracy for aggregate is **2 percent**.
- 7. The minimum and maximum limits of volume of concrete which can be mixed in a mixer are **15percent-110percent**.
- 8. The loader should remain <u>12inches</u> from the ground while removing material if stockpiles are built on the ground.

CHAPTER 6 – Concrete PLANT

- 1. **Producer'sTechnician** is responsible for designing the Concrete Mix.
- 2. <u>Producer's Technician</u> is responsible for assuring that concrete components are certified or approved.
- 3. <u>DistrictConcreteTechnician</u> is responsible for conducting the performance tests, such as yield tests.
- 4. Making the moisture correction for aggregate is the responsibility of the **Producer's Technician**.
- 5. Setting all the dials, gauges, scales, and meters at the batch plant is the responsibility of the **Producer'sTechnician**.

CHAPTER 2 – Concrete FIELD

1. What is the first step in a deck repair?

Defining the repair problem

2. What are typical causes of deterioration of concrete?

Corrosion of Reinforcement Freezing and Thawing Damage Alkali-Silica Reaction

3. What causes corrosion of reinforcement?

Chlorides

Water

Thin Concrete Cover

4. Why is corrosion of reinforcement a problem?

Causes cracks and delaminations

5. Why is poor drainage a problem?

Water and salt ponds on the surface Accelerates deterioration of concrete Promotes frost damage

6. What causes freeze thaw deterioration?

Low air content in concrete
Water expands 9.1% when it freezes

7. Why is alkali silica reaction a problem?

Alkali cement reacts with silica aggregates forming a gel around aggregates Gel absorbs water and swells Expanding gel cracks concrete

8. How do you locate deteriorated concrete caused by corrosion of reinforcement?

Chain drag
Half-cell potential measurements
Chloride content measurement

9. How do you remove concrete prior to patching?

Mark perimeter Saw cut perimeter Pneumatic hammers

10. Patching can be done with what materials?

Ready mixed concrete
Prepackaged patching materials

11. True or False. Patching should include adequate clearance under the reinforcement, saturated surface dry surface, and the use of an internal vibrator.

True

12. When should white, pigmented liquid membrane curing material be applied?

Just before the surface dries

13. How much does typical bridge deck concrete shrink in one to two years?

Approximately 1 inch per 100 feet of length

14. Concrete gains strength the fastest at what temperature?

90°F

15. What information is needed to use the evaporation rate nomograph?

Air temperature
Relative humidity
Concrete temperature
Wind speed

16. What materials do we use to fill cracks?

High molecular weight methacrylate Epoxy Urethane

17. Hydraulic cement concrete overlays should be placed on what type surface?

Shot blasted and saturated surface dry

18. What type hydraulic cement concrete overlays are used in Virginia?

Latex-modified Silica fume

19. Epoxy overlays should be placed on what type surface?

Shot blasted and dry

20. Epoxy test patches are constructed and tested to verify what is acceptable?

Materials

Surface preparation

Batching, mixing and placing materials

CHAPTER 3 – Concrete FIELD

1. What are the duties of a Hydraulic Cement Concrete Field Inspector?

To insure that construction operations produce the results called for by the plans and specifications

2. What daily records must the Hydraulic Cement Concrete Field Inspector keep?

Date, location of the work, weather conditions, test results, equipment in use, equipment idle, source of materials, and production records

3. What is a Certified Concrete Field Technician responsible for at the project site?

Quality control of concrete work

4. What is the purpose of inspection?

To keep the Engineer informed as to the progress and the manner in which the work is progressing.

5. What are the qualifications of an inspector?

Knowledge, common sense, observational skills and courtesy.

6. What is a good relationship of an Inspector with the Contractor?

The inspector should be friendly, but firm and impartial in making decisions.

7. Should an inspector know what testing is required at both the concrete plant and on the road?

Yes

8. What safety equipment should be used during road construction?

Hard hats, steel toed shoes, gloves, safety vests, protective clothing, safety glasses or anything else necessary to assure worker safety.

SpecialProvisions

Special Provision Copied Notes or Plans SpecialProvisionCopiedNotes

Between the following pairs of documents, which one has priority?

Specifications or Plans Plans

Plans or Special Provisions

9.

CHAPTER 4 - Concrete

1. When transporting concrete to the job site, how much water can be withheld and added after concrete arrives on the site?

One gallon per cubic yard

- 2. True. All forms must be mortar tight, sufficiently rigid, and oiled or wetted down before concrete placing.
- 3. The conditions which are most conducive to causing plastic shrinkage cracks are <u>high</u> winds andlowhumidity.
- 4. Exploration of the sub-foundation to determine its adequacy is done by the **Contractor**.
- 5. All forms must be treated with approved coatingmaterial or water.
- 6. It is permissible to use reinforcing steel bars with **millscaleonthem**.
- 7. Proper use of vibrator involves <u>vibratingverticallyatregularintervals</u>.
- 8. Before placing concrete on a surface, the surface should be **oiledorwetted**.
- 9. During cold weather concreting, the surface on which the concrete is to be placed should not be less than <u>40</u> °F.
- 10. The <u>Contractor</u> is responsible for removing and replacing concrete injured by frost action or freezing.
- 11. On a given day, if the air temperature was 60 °F; relative humidity 40%; surface temperature of the plastic concrete 75 °F and the wind velocity is 15 m/h, the Surface Evaporation Rate for Plastic Concrete on concrete bridge deck would be 0.25 lb/ft²/h.
- 12. The requirements for heating water, aggregates and cement in cold weather are <u>water</u> <u>andaggregates150°Fmax;cementshallnotbeheated</u>.

13. In hot weather, all efforts should be made to place the concrete at or below **theair temperature**.

- 14. Reinforcing steel bars, except those to be placed in vertical mats, shall be tied at every intersection where the spacing is more than 12 inches in any direction as found in Section 406.03(d).
- 15. When control cylinders are being used to determine removal of formwork from a deck slab, the minimum compressive strength of the deck slab is <u>60% f'c</u> as found in Section <u>404.03(j)</u>.
- 16. The requirements for the protection of reinforcing steel bars are found in Section 406.03(b).
- 17. Once concrete has begun to set in the finished surface, it shall not be disturbed or walked upon for a minimum of <a>24 hours as stated in Section <a>404.03(I)2 .
- 18. Concrete may be permitted to freely drop a maximum of <u>1.5m(5ft.)</u> as stated in Section <u>404.03(c)</u>.
- 19. Forms can be removed from a stem footer when the minimum compressive strength of the footer is 30% f'c as found in Section 404.03.
- 20. In splicing a reinforcing bar, the minimum allowable length of lap is <u>30 timesthe</u> <u>bar</u> diameter as found in Section 406.03(e).

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Calculations for Concrete Plant Study Problem

- Cement Weight Calculation (Line A 38-41)
 635 lbs. (from TL-27) x 8 cubic yards = 5,080 lbs. of cement for 8 cubic yards
- Sand, SSD Weight Calculation (Line A 46-50)
 946 lbs. (from TL-27) x 8 cubic yards. = 7,568 lbs. of sand for 8 cubic yards
- Sand, Free Water Calculation (Line A 51-53)
 7,568 lbs. of sand for 8 cubic yards x .06 (% Free Moisture of Sand Expressed as a decimal) = 454.1 lbs. of free water = 454 lbs. (rounded to nearest whole lb.)
- Coarse Aggregate (No. 57), SSD Weight Calculation (Line A 60-64)
 1,922 lbs. (From TL-27) x 8 cubic yards = 15,376 lbs. of Coarse Aggregate for 8 cubic yards
- 5. Coarse Aggregate (No. 57), Free Water Calculation (Line A 65-67)

 15,376 lbs. of C.A. (No. 57) for 8 yd³ X .002 (% Free Moist. of C.A. expressed as a decimal) = 30.8 lbs. of free water = 31 lbs. (Rounded to nearest whole lb.)
- 6. Total Allowable Water (Line B 13-16)32.5 gals. (From TL-27) x 8 cubic yards = 260.0 gals. for 8 cubic yards

NOTE: All water on Line A is in pounds, but all water on Line B is in gallons.

7. Water Added at Plant (Line B 20-23)

454 lbs. of free water in sand (Line A 51-53)

+ 31 lbs. of free water in coarse aggregate (No. 57) (Line A 65-67) 485 lbs. of free water in sand and coarse aggregate

The pounds of free water in the sand and coarse aggregate from Line A must be converted to gallons. One gallon of water weighs 8.33 lbs.

485

8.33 = 58.2 gals. of free water in sand and coarse aggregate (rounded to nearest tenth)

1 gallon of water per cubic yard is being withheld at the concrete plant on each 8 yd³ load.

1 gal. per cubic yard x 8 cubic yards = 8.0 gals. of water withheld on each 8 yd³ load

The 58.2 gals. of free water in the sand and coarse aggregate goes into the mix with this material and becomes part of the mixing water and therefore must be subtracted from the total allowable water. Also, the 8 gals. of water withheld at the plant must be subtracted from the total allowable water.

58.2 gals. of free water in the sand and coarse aggregate

+ <u>8.0</u> gals. of water withheld per load at the concrete plant 66.2 gals. of water to be subtracted from the total allowable water

260.0 gals. of total allowable water (Line B 13-16)

- 66.2 gals. of free water in sand and C.A. plus 8 gals. per load withheld at plant 193.8 gals. of water added at plant (Line B 20-23)
- 8. A. E. Admixture (Line B 31-34)

5.0 oz. (From TL-27) \times 8.0 cubic yards = 40.0 oz. for 8 cubic yards

9. Retarding Admixture (Line B 38-41)

25.0 oz. (From TL-27) x 8 cubic yards = 200.0 oz. for 8 cubic yards

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Concrete Field Study Problem Solution

Form TL-13

FORM TL-13 REV. 2/96

VIRGINIA DEPARTMENT OF TRANSPORTATION MATERIALS DIVISION NOTICE OF SHIPMENT OF CONCRETE CYLINDER

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SUBMITTED PROJECT INSPECTORS NAME